

$$F_{ae} + \frac{0.6}{Y_{II}} F_{rII} = 2\,000 + \frac{0.6}{1.6} \times 3\,931 = 3\,474\text{N}, \text{ (354kgf)}$$

$$\frac{0.6}{Y_I} F_{rI} = \frac{0.6}{0.73} \times 1\,569 = 1\,290\text{N}, \text{ (132kgf)}$$

Therefore, with this bearing arrangement, the axial load $F_{ae} + \frac{0.6}{Y_{II}} F_{rII}$ is applied on bearing I but not on bearing II.

For bearing I

$$F_{rI} = 1\,569\text{N}, \text{ (160kgf)}$$

$$F_{aI} = 3\,474\text{N}, \text{ (354kgf)}$$

since $F_{aI} / F_{rI} = 2.2 > e = 0.83$

the dynamic equivalent load $P_1 = XF_{rI} + Y_1 F_{aI}$

$$= 0.4 \times 1\,569 + 0.73 \times 3\,474$$

$$= 3\,164\text{N}, \text{ (323kgf)}$$

The fatigue life factor $f_h = f_n \frac{C_r}{P_1}$

$$= \frac{0.42 \times 38\,000}{3\,164} = 5.04$$

and the rating fatigue life $L_h = 500 \times 5.04^{\frac{10}{3}} = 109\,750\text{h}$

For bearing II

since $F_{rII} = 3\,931\text{N}$, (401kgf) , $F_{aII} = 0$

the dynamic equivalent load

$$P_{II} = F_{rII} = 3\,931\text{N}, \text{ (401kgf)}$$

the fatigue life factor

$$f_h = f_n \frac{C_r}{P_{II}} = \frac{0.42 \times 43\,000}{3\,931} = 4.59$$

and the rating fatigue life $L_h = 500 \times 4.59^{\frac{10}{3}} = 80\,400\text{h}$ are obtained.

Remarks For face-to-face arrangements (DF type), please contact NSK.

(Example 6)

Select a bearing for a speed reducer under the following conditions:

Operating conditions

Radial load $F_r = 245\,000\text{N}$, $(25\,000\text{kgf})$

Axial load $F_a = 49\,000\text{N}$, $(5\,000\text{kgf})$

Speed $n = 500\text{min}^{-1}$

Size limitation

Shaft diameter: 300mm

Bore of housing: Less than 500mm

In this application, heavy loads, shocks, and shaft deflection are expected; therefore, spherical roller bearings are appropriate.

The following spherical roller bearings satisfy the above size limitation (refer to Page B196)

d	D	B	Bearing No.	Basic dynamic load rating		Constant e	Factor Y ₃
				C _r (N)	(kgf)		
300	420	90	23960 CAE4	1 230 000	125 000	0.19	3.5
	460	118	23060 CAE4	1 920 000	196 000	0.24	2.8
	460	160	24060 CAE4	2 310 000	235 000	0.32	2.1
500	160		23160 CAE4	2 670 000	273 000	0.31	2.2
	200		24160 CAE4	3 100 000	315 000	0.38	1.8

since $F_a / F_r = 0.20 < e$
the dynamic equivalent load P is

$$P = F_r + Y_3 F_a$$

Judging from the fatigue life factor f_h in Table 5.1 and examples of applications (refer to Page A25), a value of f_h , between 3 and 5 seems appropriate.

$$f_h = f_n \frac{C_r}{P} = \frac{0.444 C_r}{F_r + Y_3 F_a} = 3 \text{ to } 5$$

Assuming that $Y_3 = 2.1$, then the necessary basic load rating C_r can be obtained

$$C_r = \frac{(F_r + Y_3 F_a) \times (3 \text{ to } 5)}{0.444} = \frac{(245\,000 + 2.1 \times 49\,000) \times (3 \text{ to } 5)}{0.444} = 2\,350\,000 \text{ to } 3\,900\,000 \text{ N}, \text{ (240\,000 to 400\,000 kgf)}$$

The bearings which satisfy this range are **23160CAE4**, and **24160CAE4**.

6. LIMITING SPEED

The speed of rolling bearings is subject to certain limits. When bearings are operating, the higher the speed, the higher the bearing temperature due to friction. The limiting speed is the empirically obtained value for the maximum speed at which bearings can be continuously operated without failing from seizure or generation of excessive heat. Consequently, the limiting speed of bearings varies depending on such factors as bearing type and size, cage form and material, load, lubricating method, and heat dissipating method including the design of the bearing's surroundings.

The limiting speeds for bearings lubricated by grease and oil are listed in the bearing tables. The limiting speeds in the tables are applicable to bearings of standard design and subjected to normal loads, i. e. $C/P \geq 12$ and $F_a/F_r \leq 0.2$ approximately. The limiting speeds for oil lubrication listed in the bearing tables are for conventional oil bath lubrication.

Some types of lubricants are not suitable for high speed, even though they may be markedly superior in other respects. When speeds are more than 70 percent of the listed limiting speed, it is necessary to select an oil or grease which has good high speed characteristics.

(Refer to)

Table 12.2 Grease Properties (Pages A110 and 111)

Table 12.5 Example of Selection of Lubricant for Bearing Operating Conditions (Page A113)

Table 15.8 Brands and Properties of Lubricating Grease (Pages A138 to A141)

6.1 Correction of Limiting Speed

When the bearing load P exceeds 8 % of the basic load rating C , or when the axial load F_a exceeds 20 % of the radial load F_r , the limiting speed must be corrected by multiplying the limiting speed found in the bearing tables by the correction factor shown in Figs. 6.1 and 6.2.

When the required speed exceeds the limiting speed of the desired bearing; then the accuracy grade, internal clearance, cage type and material, lubrication, etc., must be carefully studied in order to select a bearing capable of the required speed. In such a case, forced-circulation oil lubrication, jet lubrication, oil mist lubrication, or oil-air lubrication must be used.

If all these conditions are considered. The maximum permissible speed may be corrected by multiplying the limiting speed found in the bearing tables by the correction factor shown in Table 6.1. It is recommended that NSK be consulted regarding high speed applications.

6.2 Limiting Speed for Rubber Contact Seals for Ball Bearings

The maximum permissible speed for contact rubber sealed bearings (DDU type) is determined mainly by the sliding surface speed of the inner circumference of the seal. Values for the limiting speed are listed in the bearing tables.

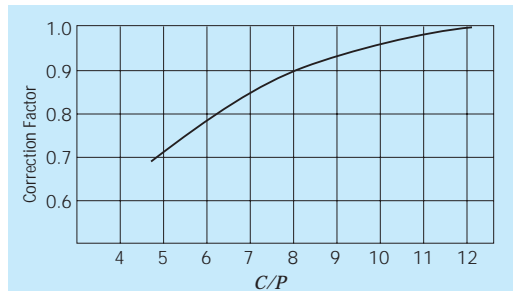


Fig. 6.1 Limiting Speed Correction Factor Variation with Load Ratio

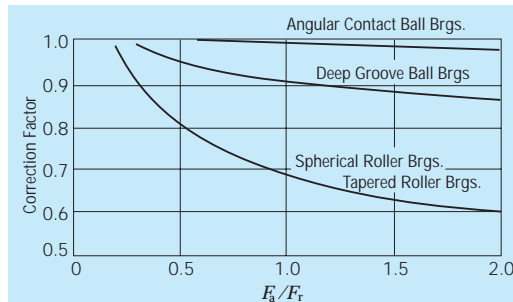


Fig. 6.2 Limiting Speed Correction Factor for Combined Radial and Axial Loads

Table 6.1 Limiting Speed Correction Factor for High-Speed Applications

Bearing Types	Correction Factor
Cylindrical Roller Brgs. (single row)	2
Needle Roller Brgs. (except broad width)	2
Tapered Roller Brgs.	2
Spherical Roller Brgs.	1.5
Deep Groove Ball Brgs.	2.5
Angular Contact Ball Brgs. (except matched bearings)	1.5