

## 15. TECHNICAL DATA

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### DEFINITIONS OF SYMBOLS AND THEIR UNITS

Symbols	Nomenclature	Units	Symbols	Nomenclature	Units
<i>a</i>	Contact Ellipse Major Axis	(mm)	<i>n<sub>a</sub></i>	Rotating Speed of Rolling Elements	(min <sup>-1</sup> )
<i>b</i>	Contact Ellipse Major Axis	(mm)	<i>n<sub>c</sub></i>	Revolving Speed of Rolling Elements (Cape Speed)	(min <sup>-1</sup> )
<i>C<sub>r</sub></i>	Basic Dynamic Load Rating of Radial Bearings	(N){kgf}	<i>n<sub>e</sub></i>	Speed of Outer Ring	(min <sup>-1</sup> )
<i>C<sub>or</sub></i>	Basic Static Load Radial of Radial Bearings	(N){kgf}	<i>n<sub>i</sub></i>	Speed of Inner Ring	(min <sup>-1</sup> )
<i>C<sub>a</sub></i>	Basic Dynamic Load Rating of Thrust Bearings	(N){kgf}	<i>p<sub>m</sub></i>	Surface Pressure on Fitted Surface	(MP <sub>a</sub> ){kgf/mm <sup>2</sup> }
<i>C<sub>oa</sub></i>	Basic Static Load Rating of Thrust Bearings	(N){kgf}	<i>P</i>	Bearing Load	(N){kgf}
<i>d</i>	Shaft Diameter, Nominal Bearing Bore Diameter	(mm)	<i>Q</i>	Rolling Element Load	(N){kgf}
<i>D</i>	Housing Bore Diameter, Nominal Bearing Outside Diameter	(mm)	<i>r<sub>e</sub></i>	Groove Radius of Outer Ring	(mm)
<i>D<sub>e</sub></i>	Outer Ring Raceway Diameter	(mm)	<i>r<sub>i</sub></i>	Groove Radius of Inner Ring	(mm)
<i>D<sub>i</sub></i>	Inner Ring Raceway Diameter	(mm)	<i>v<sub>a</sub></i>	Circumferential Speed of Rolling Element about Its Center	(m/sec)
<i>D<sub>0</sub></i>	Housing Outside Diameter	(mm)	<i>v<sub>c</sub></i>	Circumferential Speed of Rolling Element about Beading Center	(m/sec)
<i>D<sub>pw</sub></i>	Rolling Element Pitch Diameter	(mm)	<i>Z</i>	Number of Rolling Elements per Row	
<i>D<sub>w</sub></i>	Nominal Rolling Element Diameter	(mm)	<i>α</i>	Contact Angle (when axial load is applied on Radial Ball Bearing)	(°)
<i>e</i>	Contact Position of Tapered Roller End Face with Rib	(mm)	<i>α<sub>0</sub></i>	Initial Contact Angle (Geometri) (when inner and outer rings of Angular Contact Ball Bearings are pushed axially)	(°)
<i>E</i>	Modulus of Longitudinal Elasticity (Bearing Steel) 208 000 MP <sub>a</sub> {21 200 kgf/mm <sup>2</sup> }		<i>α<sub>R</sub></i>	Initial Contact Angle (Geometric) (when inner and outer rings Angular Contact Ball Bearing are pushed radially)	(°)
<i>E(k)</i>	Complete elliptic integral of the 2nd kind for which the population parameter is $k=\sqrt{1-\left(\frac{b}{a}\right)^2}$		<i>β</i>	1/2 of Conical Angle of Roller	(°)
<i>f<sub>0</sub></i>	factor which depends on the geometry of the bearing components and on the applicable stress level		<i>δ<sub>a</sub></i>	Relative Axial Displacement of Inner and Outer Rings	(mm)
<i>f(ε)</i>	Function of ε		<i>Δ<sub>a</sub></i>	Axial Internal Clearance	(mm)
<i>F<sub>a</sub></i>	Axial Load, Preload	(N){kgf}	<i>Δ<sub>d</sub></i>	Effective Interference of Inner Ring and Shaft	(mm)
<i>F<sub>r</sub></i>	Radial Load	(N){kgf}	<i>Δ<sub>r</sub></i>	Radial Internal Clearance	(mm)
<i>h</i>	$D_e/D$		<i>Δ<sub>D</sub></i>	Effective Interference of Outer Ring and Housing	(mm)
<i>h<sub>0</sub></i>	$D/D_0$		<i>Δ<sub>D<sub>e</sub></sub></i>	Contraction of Outer Ring Raceway Diameter due to Fit	(mm)
<i>k</i>	$d/D_i$		<i>Δ<sub>D<sub>i</sub></sub></i>	Expansion of Inner Ring Raceway Diameter due to Fit	(mm)
<i>K</i>	Constant Determined by Internal Design of Bearing		<i>ε</i>	Load Factor	
<i>L</i>	Fatigue Life when Effective Clearance is 0		<i>μ</i>	Coefficient of Dynamic Friction of Rolling Bearing	
<i>L<sub>we</sub></i>	Effective Length of Roller	(mm)	<i>μ<sub>e</sub></i>	Coefficient of Friction between Roller End Face and Rib	
<i>L<sub>e</sub></i>	Fatigue Life when Effective Clearance is Δ		<i>μ<sub>s</sub></i>	Coefficient of Sliding Friction	
<i>m<sub>0</sub></i>	Distance between Centers of Curvature of Inner and Outer Rings $r_i+r_e-D_w$	(mm)	<i>σ<sub>t max</sub></i>	Maximum Stress on Fitted Surfaces	(MP <sub>a</sub> ){kgf/mm <sup>2</sup> }
<i>M</i>	Frictional Torque	(N-mm){kgf-mm}			
<i>M<sub>s</sub></i>	Spin Friction	(N-mm){kgf-mm}			

## 15.1 Axial Displacement of Bearings

(1) Contact Angle  $\alpha$  and Axial Displacement  $\delta_a$  of Deep Groove Ball Bearing and Angular Contact Ball Bearings (Figs. 15.1 to 15.3)

$$\delta_a = \frac{0.00044}{\sin \alpha} \left( \frac{Q^2}{D_w} \right)^{\frac{1}{3}} \quad \text{(N)} \quad \left. \right\} (\text{mm})$$

$$\delta_a = \frac{0.002}{\sin \alpha} \left( \frac{Q^2}{D_w} \right)^{\frac{1}{3}} \quad \text{(kgf)} \quad \left. \right\}$$

$$Q = \frac{F_a}{Z \sin \alpha} \quad (\text{N}), \quad \{\text{kgf}\}$$

(2) Axial Load  $F_a$  and Axial Displacement  $\delta_a$  of Tapered Roller Bearings (Fig. 15.4)

$$\delta_a = \frac{0.000077 F_a^{0.9}}{(\sin \alpha)^{1.9} Z^{0.9} L_{we}^{0.8}} \quad \text{(N)} \quad \left. \right\} (\text{mm})$$

$$\delta_a = \frac{0.0006 F_a^{0.9}}{(\sin \alpha)^{1.9} Z^{0.9} L_{we}^{0.8}} \quad \text{(kgf)} \quad \left. \right\}$$

### Remarks:

Actual axial displacement may vary depending on the shaft/housing thickness, material, and fitting interference with the bearing. Please contact NSK about such factors of axial displacement which are not discussed in detail in this catalog.

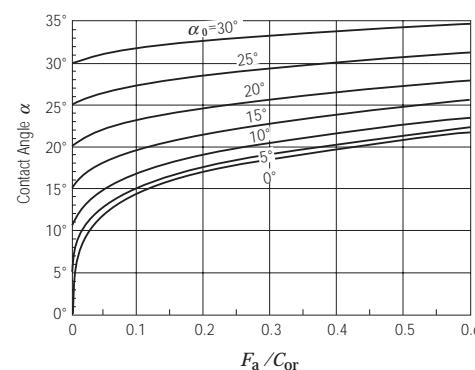


Fig. 15.1  $F_a / C_{\text{Or}}$  and Contact Angle of Deep Groove and Angular Contact Ball Bearings

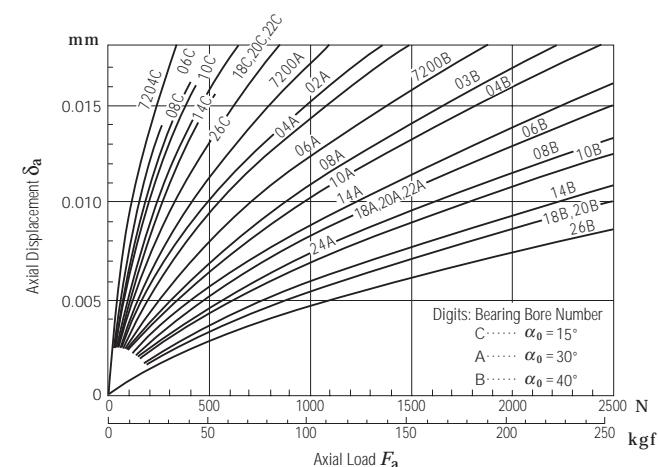


Fig. 15.3 Axial Load and Axial Displacement of Angular Contact Ball Bearings

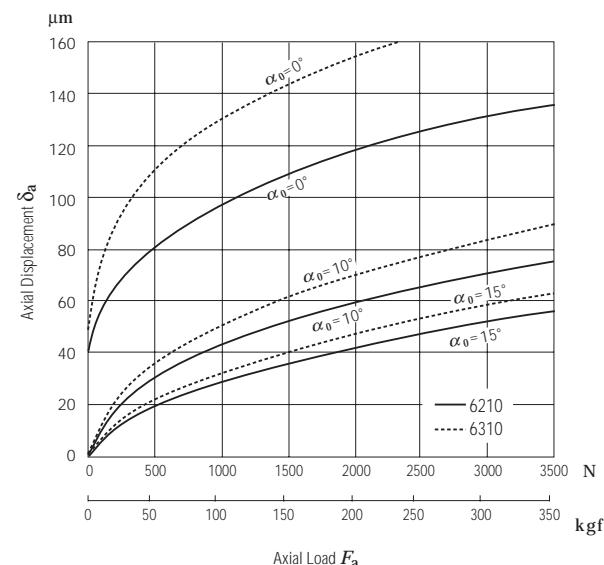


Fig. 15.2 Axial Load and Axial Displacement of Deep Groove Ball Bearings

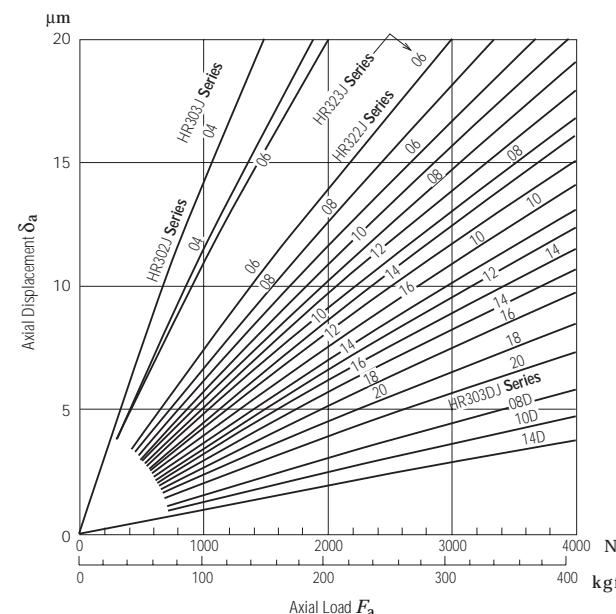


Fig. 15.4 Axial Load and Axial Displacement of Tapered Roller Bearings

## 15.2 Fits

(1) Surface Pressure  $p_m$ , Maximum Stress  $\sigma_{t\max}$  on Fitted Surfaces and Expansion or Contraction of Inner Ring Raceway Diameter  $\Delta D_i$  or Contraction of Outer Ring Raceway Diameter  $\Delta D_e$  (Table 15.1, Figs. 15.5 and 15.6)

(2) Interferences or Clearances of Shafts and Inner Rings (Table 15.2)

(3) Interferences or Clearances of Housing Bores and Outer Rings (Table 15.3)

Table. 15. 1 Surface Pressure, Maximum Stress on Fitted Surfaces and Expansion or Contraction

Items	Shaft & Inner Ring	Housing & Bore & Outer Ring
Surface Pressure $p_m$ (MPa) {kgf/mm²}	(In case of solid shaft) $p_m = \frac{E}{2} \frac{\Delta d}{D} (1 - k^2)$	In case of housing outside dia. $D_0 \neq \infty$ $p_m = \frac{E}{2} \frac{\Delta D}{D} \frac{(1 - h^2)}{1 - h^2 h_0^2}$
Maximum stress $\sigma_{t\max}$ (MPa) {kgf/mm²}	Maximum circumferential stress on fitted surface of inner ring bore is $\sigma_{t\max} = p_m \frac{1 + k^2}{1 - k^2}$	Maximum circumferential stress on outer ring bore surface is $\sigma_{t\max} = p_m \frac{2}{1 - h^2}$
Expansion of inner ring raceway dia. $\Delta D_i$ (mm)	In case of solid shaft $\Delta D_i = \Delta d \cdot k$	In case $D_0 \neq \infty$ $\Delta D_o = \Delta D \cdot h \frac{1 - h_0^2}{1 - h^2 h_0^2}$
Contraction of outer ring raceway dia. $\Delta D_e$ (mm)		In case $D_0 = \infty$ $\Delta D_e = \Delta D \cdot h$

Remarks The modulus of longitudinal elasticity and Poisson's ratio for the shaft and housing material are the same as those for inner and outer rings.

Reference 1 MPa=1 N/mm²=0.102 kgf/mm²

Table 15. 2 Interferences or Clearances

Size Classification (mm)	Single Plane Mean Bore Dia. Deviation (Normal) $\Delta d_{mp}$	Interferences or Clearances for													
		f6		g5		g6		h5		h6		js5		j5	
		Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference
over	incl.	high	low	max.	min.	max.	max.								
3	6	0	-8	18	2	9	4	12	4	5	8	8	—	—	—
6	10	0	-8	22	5	11	3	14	3	6	8	9	8	3	11
10	18	0	-8	27	8	14	2	17	2	8	8	11	8	4	12
18	30	0	-10	33	10	16	3	20	3	9	10	13	10	4.5	14.5
30	50	0	-12	41	13	20	3	25	3	11	12	16	12	5.5	17.5
50	65	0	-15	49	15	23	5	29	5	13	15	19	15	6.5	21.5
65	80	0	-15	49	15	23	5	29	5	13	15	19	15	6.5	21.5
80	100	0	-20	58	16	27	8	34	8	15	20	22	20	7.5	27.5
100	120	0	-20	58	16	27	8	34	8	15	20	22	20	7.5	27.5
120	140	0	-25	68	18	32	11	39	11	18	25	25	9	34	11
140	160	0	-25	68	18	32	11	39	11	18	25	25	9	34	11
160	180	0	-25	68	18	32	11	39	11	18	25	25	9	34	11
180	200	0	-30	79	20	35	15	44	15	20	30	29	30	10	40
200	225	0	-30	79	20	35	15	44	15	20	30	29	30	10	40
225	250	0	-30	79	20	35	15	44	15	20	30	29	30	10	40
250	280	0	-35	88	21	40	18	49	18	23	35	32	35	11.5	46.5
280	315	0	-35	88	21	40	18	49	18	23	35	32	35	11.5	46.5
315	355	0	-40	98	22	43	22	54	22	25	40	36	40	12.5	52.5
355	400	0	-40	98	22	43	22	54	22	25	40	36	40	12.5	52.5
400	450	0	-45	108	23	47	25	60	25	27	45	40	45	13.5	58.5
450	500	0	-45	108	23	47	25	60	25	27	45	40	45	13.5	58.5

- Remarks 1. The figures for tolerance classes where stress caused by the fitting of the shaft and inner ring becomes excessive are omitted.  
2. The tolerance range js is now recommended instead of j.

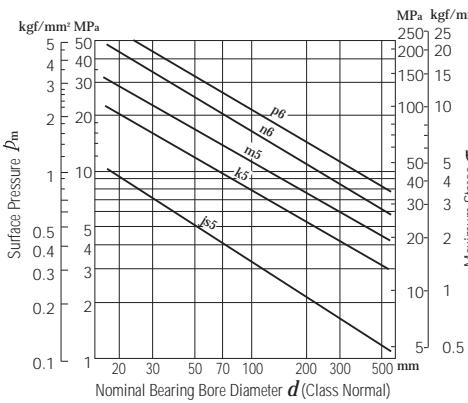


Fig. 15.5 Surface Pressure  $P_m$  and Maximum Stress  $\sigma_{t\max}$  for Average Fitting Interference

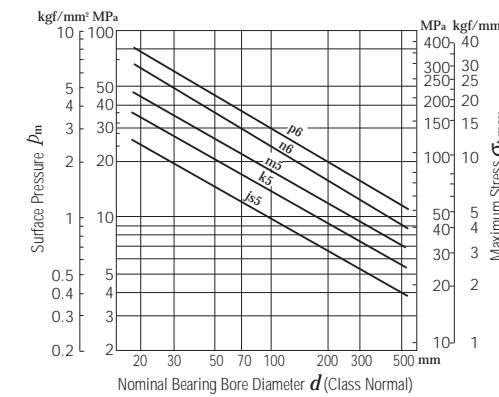


Fig. 15.6 Surface Pressure  $P_m$  and Maximum Stress  $\sigma_{t\max}$  for Maximum Fitting Interference

of Shafts and Inner Rings

Units : μm

Size Classification (mm)	Single Plane Mean Bore Dia. Deviation (Normal) $\Delta d_{mp}$	Each Fitting Class														Size Classification (mm)			
		js6		j6		k5		k6		m5		m6		n6		p6		r6	
		Clearance	Interference	Clearance	Interference	Interference													
over	incl.	max.	max.	max.	max.	min.	max.												
3	6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	3	6		
6	10	4.5	12.5	2	15	—	—	—	—	—	—	—	—	—	—	—	6	10	
10	18	5.5	13.5	3	16	—	—	—	—	—	—	—	—	—	—	—	10	18	
18	30	6.5	16.5	4	19	2	21	2	25	—	—	—	—	—	—	—	18	30	
30	50	8	20	5	23	2	25	2	30	9	32	9	37	—	—	—	30	50	
50	65	9.5	24.5	7	27	2	30	2	36	11	39	11	45	—	—	—	50	65	
65	80	9.5	24.5	7	27	2	30	2	36	11	39	11	45	20	54	—	65	80	
80	100	11	31	9	33	3	38	3	45	13	48	13	55	23	65	37	80	100	
100	120	11	31	9	33	3	38	3	45	13	48	13	55	23	65	37	100	120	
120	140	12.5	37.5	11	39	3	46	3	53	15	58	15	65	27	77	43	93	113	
140	160	12.5	37.5	11	39	3	46	3	53	15	58	15	65	27	77	43	93	115	
160	180	12.5	37.5	11	39	3	46	3	53	15	58	15	65	27	77	43	93	115	
180	200	14.5	44.5	13	46	4	54	4	63	17	67	17	76	31	90	50	109	136	
200	225	14.5	44.5	13	46	4	54	4	63	17	67	17	76	31	90	50	109	139	
225	250	14.5	44.5	13	46	4	54	4	63	17	67	17	76	31	90	50	109	143	
250	280	16	51	16	51	4	62	4	71	20	78	20	87	34	101	56	123	94	
280	315	16	51	16	51	4	62	4	71	20	78	20	87	34	101	56	123	98	
315	355	18	58	18	58	4	69	4	80	21	86	21	97	37	113	62	138	108	
355	400	18	58	18	58	4	69	4	80	21	86	21	97	37	113	62	138	190	
400	450	20	65	20	65	5	77	5	90	23	95	23	108	40	125	68	153	217	
450	500	20	65	20	65	5	77	5	90	23	95	23	108	40	125	68	153	217	

Table 15. 3 Interferences or Clearances of Housing Bores and Outer Rings

Units :  $\mu\text{m}$ 

Size Classification (mm)	Single Plane Mean O. D. Deviation (Normal) $\Delta D_{\text{imp}}$	Interferences or Clearances for														
		G7		H6		H7		H8		J6		JS6		J7		
		Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	
over	incl.	high	low	max.	min.	max.										
6	10	0	-	8	28	5	17	0	23	0	13	4	12.5	4.5	16	7
10	18	0	-	8	32	6	19	0	26	0	35	0	14	5	13.5	5.5
18	30	0	-	9	37	7	22	0	30	0	42	0	17	5	15.5	6.5
30	50	0	-	11	45	9	27	0	36	0	50	0	21	6	19	8
50	80	0	-	13	53	10	32	0	43	0	59	0	26	6	22.5	9.5
80	120	0	-	15	62	12	37	0	50	0	69	0	31	6	26	11
120	150	0	-	18	72	14	43	0	58	0	81	0	36	7	30.5	12.5
150	180	0	-	25	79	14	50	0	65	0	88	0	43	7	37.5	12.5
180	250	0	-	30	91	15	59	0	76	0	102	0	52	7	44.5	14.5
250	315	0	-	35	104	17	67	0	87	0	116	0	60	7	51	16
315	400	0	-	40	115	18	76	0	97	0	129	0	69	7	58	18
400	500	0	-	45	128	20	85	0	108	0	142	0	78	7	65	20
500	630	0	-	50	142	22	94	0	120	0	160	0	—	—	72	22
630	800	0	-	75	179	24	125	0	155	0	200	0	—	—	100	25
800	1000	0	-	100	216	26	156	0	190	0	240	0	—	—	128	28

Note (\*) Indicates the minimum interference

Remarks The tolerance range JS is now recommended instead of J.

### 15.3 Radial and Axial Internal Clearances

(1) Radial Internal Clearance  $\Delta_r$  and Axial Internal Clearance  $\Delta_a$  in Single-Row Deep Groove Ball Bearings (Fig. 15.7)

$$\Delta_a = K \Delta_r^{\frac{1}{2}} \quad (\text{mm})$$

where

$$K = 2 (r_e + r_i - D_w)^{\frac{1}{2}}$$

(2) Radial Internal Clearance  $\Delta_r$  and Axial Internal Clearance  $\Delta_a$  in Double-Row Angular Contact Ball Bearings (Fig. 15.8)

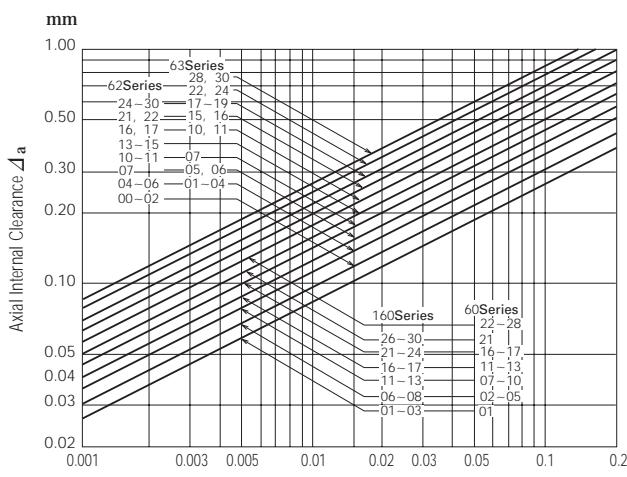
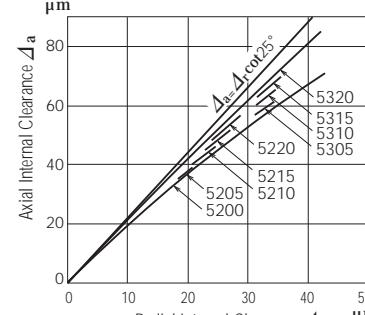
$$\Delta_a = 2 \sqrt{m_0^2 - (m_0 \cos \alpha_R - \frac{\Delta_r}{2})^2} - 2 m_0 \sin \alpha_R \quad (\text{mm})$$

Table 15. 4 Constant  $K$ 

Bore No.	160XX	60XX	62XX	63XX
00	—	—	0.93	1.14
01	0.80	0.80	0.93	1.06
02	0.80	0.93	0.93	1.06
03	0.80	0.93	0.99	1.11
04	0.90	0.96	1.06	1.07
05	0.90	0.96	1.06	1.20
06	0.96	1.01	1.07	1.19
07	0.96	1.06	1.25	1.37
08	0.96	1.06	1.29	1.45
09	1.01	1.11	1.29	1.57
10	1.01	1.11	1.33	1.64
11	1.06	1.20	1.40	1.70
12	1.06	1.20	1.50	2.09
13	1.06	1.20	1.54	1.82
14	1.16	1.29	1.57	1.88
15	1.16	1.29	1.57	1.95
16	1.20	1.37	1.64	2.01
17	1.20	1.37	1.70	2.06
18	1.29	1.44	1.76	2.11
19	1.29	1.44	1.82	2.16
20	1.29	1.44	1.88	2.25
21	1.37	1.54	1.95	2.32
22	1.40	1.64	2.01	2.40
24	1.40	1.64	2.06	2.40
26	1.54	1.70	2.11	2.49
28	1.54	1.70	2.11	2.59
30	1.57	1.76	2.11	2.59

Table 15. 3 Interferences or Clearances of Housing Bores and Outer Rings

Each Fitting Class														Size Classification (mm)			
JS7		K6		K7		M6		M7		N6		N7		P6		P7	
Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference	Clearance	Interference
max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.	max.
15	7	10	7	13	10	5	12	8	15	1	16	4	19	4	21	1	24
17	9	10	9	14	12	4	15	8	18	1*	20	3	23	7	26	3	29
19	10	11	11	15	15	5	17	9	21	2*	24	2	28	9	31	5	35
23	12	14	13	18	18	7	20	11	25	1*	28	3	33	10	37	6	42
28	15	17	15	22	21	8	24	13	30	1*	33	4	39	13	45	8	51
32	17	19	18	25	25	9	28	15	35	1*	38	5	45	15	52	9	59
38	20	22	21	30	28	10	33	18	40	2*	45	6	52	18	61	10	68
45	20	29	21	37	28	17	33	25	40	5	45	13	52	11	61	3	68
53	23	35	24	43	33	22	37	30	46	8	51	16	60	11	70	3	180
61	26	40	27	51	36	26	41	35	52	10	57	21	66	12	79	1	88
68	28	47	29	57	40	30	46	40	57	14	62	24	73	11	87	1	98
76	31	53	32	63	45	35	50	45	63	18	67	28	80	10	95	0	108
85	35	50	44	50	70	24	70	24	96	6	88	6	114	28	122	28	148
115	40	75	50	75	80	45	80	45	110	25	100	25	130	13	138	13	168
145	45	100	56	100	90	66	90	66	124	44	112	44	146	0	156	0	190

Fig. 15.7  $\Delta_r$  and  $\Delta_a$  in Single-Row Deep Groove Ball BearingsFig. 15.8  $\Delta_r$  and  $\Delta_a$  in Double-Row Angular Contact Ball Bearings (52, 53 Series)

## 15. 4 Preload and Starting Torque

(1) Axial Load  $F_a$  and Starting Torque  $M$  of Tapered Roller Bearings (Figs. 15.9 and 15.10)

$$M = e \mu_e F_a \cos\beta \quad (\text{N}\cdot\text{mm}, \{\text{kgf}\cdot\text{mm}\})$$

where

$$\mu_e : 0.20$$

When bearings with the same number are used in opposition, the torque  $M$  caused by the preload becomes  $2M$ .

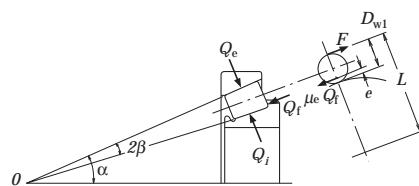


Fig. 15.9 Relation between  $e$  and  $\beta$

(2) Preload  $F_a$  and Starting Torque  $M$  of Angular Contact Ball Bearings and Double-Direction Angular Contact Thrust Ball Bearings (Figs. 15.11 and 15.12)

$$M = M_s Z \sin\alpha \quad (\text{N}\cdot\text{mm}, \{\text{kgf}\cdot\text{mm}\})$$

where  $M_s$  is spin friction

$$M_s = \frac{3}{8} \mu_s Q a E(k) \quad (\text{N}\cdot\text{mm}, \{\text{kgf}\cdot\text{mm}\})$$

where

$$\mu_s = 0.15$$

When bearings with the same number are used in opposition, the torque  $M$  caused by the preload becomes  $2M$ .

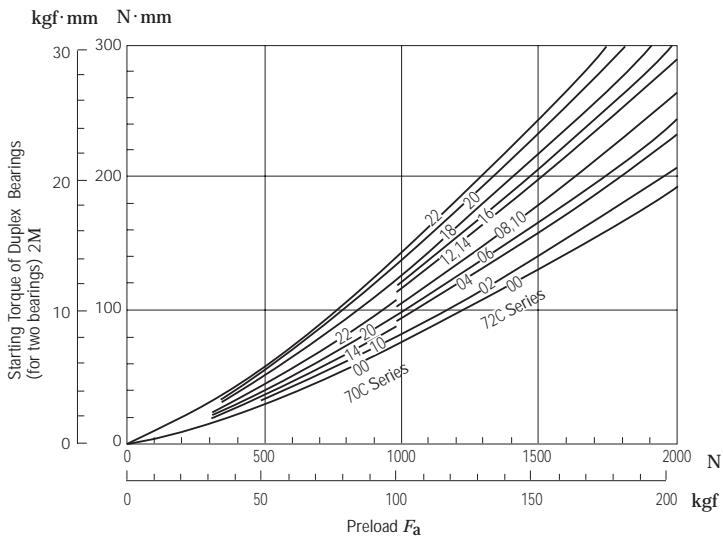


Fig. 15.11 Preload and Starting Torque for Back-to-Back or Face-to-Face Arrangements of Angular Contact Ball Bearings ( $\alpha = 15^\circ$ )

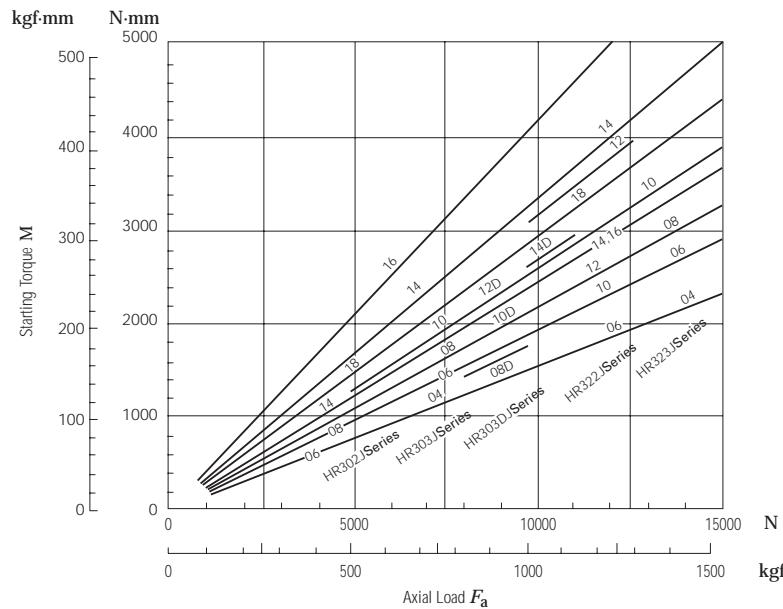


Fig. 15.10 Relation between Axial Load and Starting Torque of Tapered Roller Bearings

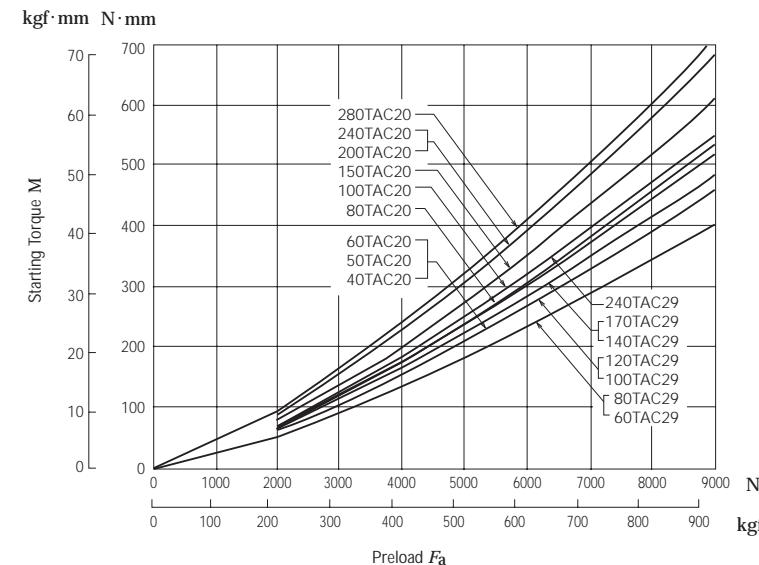


Fig. 15.12 Preload and Starting Torque of Double-Direction Angular Contact Thrust Ball Bearings

## 15.5 Coefficients of Dynamic Friction and Other Bearing Data

### (1) Bearing Types and Their Coefficients of Dynamic Friction $\mu$

$$\mu = \frac{M}{P \cdot \frac{d}{2}}$$

Table 15.5 Coefficients of Dynamic Friction

Bearing Types	Approximate values of $\mu$
Deep Groove Ball Bearings	0.0013
Angular Contact Ball Bearings	0.0015
Self-Aligning Ball Bearings	0.0010
Thrust Ball Bearings	0.0011
Cylindrical Roller Bearings	0.0010
Tapered Roller Bearings	0.0022
Spherical Roller Bearings	0.0028
Needle Roller Bearings with Cages	0.0015
Full Complement Needle Roller Bearings	0.0025
Spherical Thrust Roller Bearings	0.0028

### (3) Radial Internal Clearance $\Delta_r$ and Fatigue Life $L$ (Fig. 15.13)

For the radial internal clearance  $\Delta_r$  and the function  $f(\varepsilon)$  of the load factor, the following equations are valid:

For Deep Groove Ball Bearings

$$f(\varepsilon) = \frac{\Delta_r \cdot D_w^{1/3}}{0.00044 \left( \frac{F_r}{Z} \right)^{2/3}} \quad \text{(N)}$$

$$f(\varepsilon) = \frac{\Delta_r \cdot D_w^{1/3}}{0.002 \left( \frac{F_r}{Z} \right)^{2/3}} \quad \text{(kgf)}$$

For Cylindrical Roller Bearings

$$f(\varepsilon) = \frac{\Delta_r \cdot L_{we}^{0.8}}{0.000077 \left( \frac{F_r}{Z} \right)^{0.9}} \quad \text{(N)}$$

$$f(\varepsilon) = \frac{\Delta_r \cdot L_{we}^{0.8}}{0.0006 \left( \frac{F_r}{Z} \right)^{0.9}} \quad \text{(kgf)}$$

The relation between the load factor  $\varepsilon$  and  $f(\varepsilon)$  and  $L_e/L$ , when the radial internal clearance is  $\Delta_r$  is as shown in Table 15.7.

From the above equations, first obtain  $f(\varepsilon)$  and then  $\varepsilon$  and  $L_e/L$  can be obtained.

### (2) Circumferential Speeds of Rolling Elements about Their Centers and Bearing Center

Table 15.6 Circumferential Speeds of Rolling Elements about Their Centers and Bearing Center

Items	Rotating inner ring, fixed outer ring	Rotating outer ring, fixed inner ring
Ball rotating speed $n_a$ (min <sup>-1</sup> )	$-\left( \frac{D_{pw}}{D_w} - \frac{\cos^2\alpha}{D_{pw}/D_w} \right) \frac{n_i}{2}$	$+\left( \frac{D_{pw}}{D_w} - \frac{\cos^2\alpha}{D_{pw}/D_w} \right) \frac{n_e}{2}$
Circumferential speed around bearing ball's center $v_a$ (m/sec)	$-\frac{\pi \cdot D_w}{60 \times 10^3} \left( \frac{D_{pw}}{D_w} - \frac{\cos^2\alpha}{D_{pw}/D_w} \right) \frac{n_i}{2}$	$+\frac{\pi \cdot D_w}{60 \times 10^3} \left( \frac{D_{pw}}{D_w} - \frac{\cos^2\alpha}{D_{pw}/D_w} \right) \frac{n_e}{2}$
Revolving speed around bearing center $n_c$ (min <sup>-1</sup> )	$+ \left( 1 - \frac{\cos \alpha}{D_{pw}/D_w} \right) \frac{n_i}{2}$	$+ \left( 1 - \frac{\cos \alpha}{D_{pw}/D_w} \right) \frac{n_e}{2}$
Circumferential speed around bearing center $v_c$ (m/sec)	$-\frac{\pi \cdot D_{pw}}{60 \times 10^3} \left( 1 - \frac{\cos \alpha}{D_{pw}/D_w} \right) \frac{n_i}{2}$	$+\frac{\pi \cdot D_{pw}}{60 \times 10^3} \left( 1 - \frac{\cos \alpha}{D_{pw}/D_w} \right) \frac{n_e}{2}$

Remarks 1. + sign indicates CW rotation and - sign CCW

2. The revolving speed and circumferential speed of the rolling elements are the same as those of the cage.

Table 15.7  $\varepsilon$  and  $f(\varepsilon)$ ,  $L_e/L$ 

$\varepsilon$	Deep Groove Ball Bearings		Cylindrical Roller Bearings	
	$f(\varepsilon)$	$\frac{L_e}{L}$	$f(\varepsilon)$	$\frac{L_e}{L}$
0.1	33.713	0.294	51.315	0.220
0.2	10.221	0.546	14.500	0.469
0.3	4.045	0.737	5.539	0.691
0.4	1.408	0.889	1.887	0.870
0.5	0	1.0	0	1.0
0.6	-0.859	1.069	-1.133	1.075
0.7	-1.438	1.098	-1.897	1.096
0.8	-1.862	1.094	-2.455	1.065
0.9	-2.195	1.041	-2.929	0.968
1.0	-2.489	0.948	-3.453	0.805
1.25	-3.207	0.605	-4.934	0.378
1.5	-3.877	0.371	-6.387	0.196
1.67	-4.283	0.276	-7.335	0.133
1.8	-4.596	0.221	-8.082	0.100
2.0	-5.052	0.159	-9.187	0.067
2.5	-6.114	0.078	-11.904	0.029
3	-7.092	0.043	-14.570	0.015
4	-8.874	0.017	-19.721	0.005
5	-10.489	0.008	-24.903	0.002
10	-17.148	0.001	-48.395	0.0002

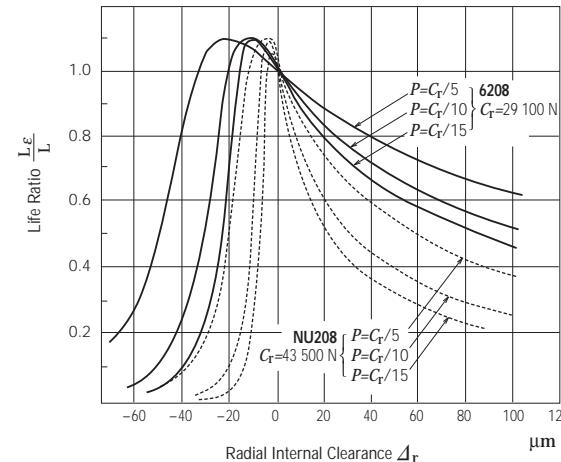


Fig. 15.13 Radial Internal Clearance and Life Ratio

## 15. 6 BRANDS AND PROPERTIES OF LUBRICATING GREASES

Table 15. 8 Brands of Lubricating Greases

Brands	Thickeners	Base Oils
ADLEX	Lithium	Mineral oil
APOOIL AUTOLEX A	Lithium	Mineral oil
ARAPEN RB 300	Lithium/Calcium	Mineral oil
EA2 GREASE	Urea (¹)	Poly- $\alpha$ -olefin oil
EA3 GREASE	Urea (¹)	Poly- $\alpha$ -olefin oil
EA5 GREASE	Urea (¹)	Poly- $\alpha$ -olefin oil
EA7 GREASE	Urea (¹)	Poly- $\alpha$ -olefin oil
ENC GREASE	Urea (¹)	Polyol ester oil + Mineral oil (²)
ENS GREASE	Urea (¹)	Polyol ester oil (³)
ECE GREASE	Lithium	Poly- $\alpha$ -olefin oil
ISOFLEX NBU 15	Barium Complex	Ester oil + Mineral oil (⁴)
ISOFLEX SUPER LDS 18	Lithium	Ester oil (⁴)
ISOFLEX TOPAS NB 52	Barium Complex	Poly- $\alpha$ -olefin oil
DOW CORNING SH 33 L GREASE	Lithium	Silicone oil (⁵)
DOW CORNING SH 44 M GREASE	Lithium	Silicone oil (⁵)
NS HI-LUBE	Lithium	Polyol ester oil + Diester oil (⁶)
NSC GREASE	Lithium	Alkyldiphenyl ether oil + Polyol ester oil (⁷)
NSK CLEAN GREASE LG2	Lithium	Poly- $\alpha$ -olefin oil + Mineral oil
EMALUBE 8030	Urea (¹)	Mineral oil
MAB GREASE	Urea (¹)	Alkyldiphenyl ether oil + Poly- $\alpha$ -olefin oil
KRYTOX GPL-524	PTFE	Perfluoropolyether oil
KP1 GREASE	PTFE	Perfluoropolyether oil
COSMO WIDE GREASE WR No.3N	Sodium Terephthalamate	Polyol ester oil + Mineral oil (⁸)
G-40M	Lithium	Silicone oil (⁹)
SHELL GADUS S2 V220 2	Lithium	Mineral oil
SHELL ALVANIA GREASE S1	Lithium	Mineral oil
SHELL ALVANIA GREASE S2	Lithium	Mineral oil
SHELL ALVANIA GREASE S3	Lithium	Mineral oil
CASSIDA GREASE RLS 2	Aluminum Complex	Poly- $\alpha$ -olefin oil
SHELL SUNLIGHT GREASE 2	Lithium	Mineral oil
WPH GREASE	Urea (¹)	Poly- $\alpha$ -olefin oil
DEMNUN GREASE L-200	PTFE	Perfluoropolyether oil
NIGACE WR-S	Urea (¹)	Synthetic oil
NIGLUBE RSH	Sodium Complex	Polyalkylene Glycol oil

Notes (¹) If grease will be used at the upper or lower limit sufficient of the temperature range or in a special environment such as vacuum, it is advisable to consult NSK.

(²) For short-term operation or when cooling is grease may be used at speeds exceeding the above limits provided the supply of grease is appropriate.

(³) Urea-based grease causes fluorine-based material to deteriorate.

(⁴) Ester-based grease causes acrylic rubber material to swell.

(⁵) Silicone-based grease causes silicone-based material to swell.

## and Comparison of Properties

Dropping Point (°C)	Consistency	Working Temperature Range(¹)(°C)	Pressure Resistance	Usable Limit Compared to Listed Limiting Speed(²)(%)
198	300	0 to +110	Good	70
198	280	-10 to +110	Fair	60
177	294	-10 to + 80	Fair	70
≥ 260	243	-40 to +150	Fair	100
≥ 260	230	-40 to +150	Fair	100
≥ 260	251	-40 to +160	Good	60
≥ 260	243	-40 to +160	Fair	100
≥ 260	262	-40 to +160	Fair	70
≥ 260	264	-40 to +160	Poor	100
≥ 260	235	-10 to +120	Fair	100
≥ 260	280	-30 to +120	Poor	100
195	280	-50 to +110	Poor	100
≥ 260	280	-40 to +130	Poor	90
210	310	-60 to +120	Poor	60
210	260	-30 to +130	Poor	60
192	250	-40 to +130	Fair	100
192	235	-30 to +140	Fair	70
201	199	-40 to +130	Poor	100
≥ 260	280	0 to +130	Good	60
≥ 260	283	-30 to +160	Fair	70
≥ 260	265	0 to +200	Fair	70
≥ 260	280	-30 to +200	Fair	60
≥ 230	227	-40 to +130	Poor	100
223	252	-30 to +130	Poor	60
187	276	0 to + 80	Good	60
182	323	-10 to +110	Fair	70
185	275	-10 to +110	Fair	70
185	242	-10 to +110	Fair	70
≥ 240	280	0 to +120	Fair	70
200	274	-10 to +110	Fair	70
259	240	-40 to +150	Fair	70
≥ 260	280	-30 to +200	Fair	60
≥ 260	230	-30 to +150	Poor	70
≥ 260	270	-20 to +120	Fair	60

(continued on next page)

Brands	Thickeners	Base Oils
PALMAX RBG	Lithium Complex	Mineral oil
BEACON 325	Lithium	Diester oil (⁹)
MULTEMP PS No.2	Lithium	Poly- $\alpha$ -olefin oil + Diester oil (⁹)
MOLYKOTE FS-3451 GREASE	PTFE	Fluorosilicone oil (⁹)
UME GREASE	Urea	Mineral oil
RAREMAX AF-1	Urea	Mineral oil

- Notes**
- (¹) If grease will be used at the upper or lower limit sufficient of the temperature range or in a special environment such as vacuum, it is advisable to consult NSK.
  - (²) For short-term operation or when cooling is grease may be used at speeds exceeding the above limits provided the supply of grease is appropriate.
  - (³) Urea-based grease causes fluorine-based material to deteriorate.
  - (⁴) Ester-based grease causes acrylic rubber material to swell.
  - (⁵) Silicone-based grease causes silicone-based material to swell.

Dropping Point (°C)	Consistency	Working Temperature Range(¹)(°C)	Pressure Resistance	Usable Limit Compared to Listed Limiting Speed(²)(%)
216	300	-10 to +130	Good	70
190	274	-50 to +100	Poor	100
190	275	-50 to +110	Poor	100
≥ 260	285	0 to +180	Fair	70
≥ 260	268	-10 to +130	Fair	70
≥ 260	300	-10 to +130	Fair	70